

LES of Turbulent Flows: Lectures 8 and 9

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- 1 LES filtered equations for compressible flows



- What if we apply a filter to the compressible Navier-Stokes equations? Let's look at mass continuity as an example.

$$\overline{\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i}} = 0$$

$$\frac{\partial \widetilde{\rho}}{\partial t} + \frac{\partial \widetilde{\rho u_i}}{\partial x_i} = 0$$

$$\frac{\partial \widetilde{\rho}}{\partial t} + \frac{\partial \widetilde{\rho u_i}}{\partial x_i} = 0$$

- We end up with a SFS term involving density, $\widetilde{\rho u_i}$, which requires modeling.
- How do we avoid this?



Density-weighted filtering

- Density-weighted filtering was formalized by Favre (1983) for ensemble statistics.
- The procedure is often referred to as Favre filtering.
- For an arbitrary quantity ϕ , the Favre filter is applied as:

$$\bar{\phi} = \frac{\widetilde{\rho\phi}}{\widetilde{\rho}} \Rightarrow \widetilde{\rho\phi} = \widetilde{\rho}\bar{\phi}$$

- As we approach incompressibility, $\bar{\phi} \sim \widetilde{\phi}$
- For LES purposes, the Favre filter represents a density-weighted spatial average.



Non-dimensional compressible equations of motion

- Non-dimensionalize

$$u_i^* = \frac{u_i}{U}$$

$$x_i^* = \frac{x_i}{\ell}$$

$$p^* = \frac{p}{\rho_o U^2} = \frac{p\ell}{\mu_o U}$$

$$t^* = \frac{tU}{\ell}$$

$$\theta^* = \frac{\theta}{\theta_o}$$

$$\nu^* = \frac{\nu}{\nu_o}$$

$$\mu^* = \frac{\mu}{\mu_o}$$

,

where the $*$ denotes a non-dimensionalized term.



- Apply Favre filter to mass continuity:

$$\overbrace{\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i}} = 0 \Rightarrow \frac{\partial \tilde{\rho}}{\partial t} + \frac{\partial \tilde{\rho} \tilde{u}_i}{\partial x_i} = 0$$

- Recall that the Favre filter is applied as: $\tilde{\rho \phi} = \tilde{\rho} \bar{\phi}$.
- Substitution yields the Favre-filtered mass continuity equation:

$$\frac{\partial \tilde{\rho}}{\partial t} + \frac{\partial (\tilde{\rho} \bar{u}_i)}{\partial x_i} = 0$$



- Next, let's rewrite in non-dimensional terms

$$\frac{\partial \tilde{\rho}}{\partial t} + \frac{\partial(\tilde{\rho}\bar{\phi})}{\partial x_i} = \cancel{\frac{\rho_o U}{\ell} \frac{\partial \tilde{\rho}^*}{\partial t^*}} + \cancel{\frac{\rho_o U}{\ell} \frac{\partial \tilde{\rho}^* \bar{u}_i^*}{\partial x_i^*}} = 0$$

The result is the non-dimensional Favre-filtered mass continuity equation

$$\boxed{\frac{\partial \tilde{\rho}}{\partial t} + \frac{\partial(\tilde{\rho}\bar{u}_i)}{\partial x_i} = 0}$$

where we have dropped the * notation for convenience.



Favre-filtered conservation of momentum

- Start with the conservation of mass:

$$\underbrace{\frac{\partial(\rho u_i)}{\partial t}}_1 + \underbrace{\frac{\partial(\rho u_i u_j)}{\partial x_j}}_2 = - \underbrace{\frac{\partial p}{\partial x_i}}_3 + \underbrace{\frac{\partial}{\partial x_j} \left[2\mu S_{ij} - \frac{2}{3}\mu\delta_{ij} \frac{\partial u_k}{\partial x_k} \right]}_4$$

- To make life easier, let's filter each term individually.



Favre-filtered conservation of momentum

- Term 1

$$\frac{\widetilde{\partial(\rho u_i)}}{\partial t} = \frac{\partial(\widetilde{\rho u_i})}{\partial t} = \frac{\partial(\widetilde{\rho} \widetilde{u_i})}{\partial t}$$

Non-dimensionalizing yields

$$\frac{\partial(\widetilde{\rho} \widetilde{u_i})}{\partial t} = \frac{(\partial \widetilde{\rho}^* \rho_o \widetilde{u_i}^* U)}{\partial t^* \ell / U} = \boxed{\frac{\rho_o U^2}{\ell} \frac{\partial(\widetilde{\rho} \widetilde{u_i})}{\partial t}}$$

where we have dropped the * notation for convenience.



Favre-filtered conservation of momentum

- Term 2

$$\frac{\overline{\partial(\rho u_i u_j)}}{\partial x_j} = \frac{\partial(\overline{\rho u_i u_j})}{\partial x_j} = \frac{\partial(\tilde{\rho} \overline{u_i u_j})}{\partial x_j}$$

Recall from our derivation of the incompressible momentum equation that we utilized the Leonard (1974) decomposition:

$$\widetilde{u_i u_j} = \tilde{u}_i \tilde{u}_j + \tau_{ij}$$

where τ_{ij} is the SFS stress tensor. Similarly

$$\overline{u_i u_j} = \overline{u}_i \overline{u}_j + \tau_{ij}$$

where we have dropped the * notation for convenience.



Favre-filtered conservation of momentum

- Term 2

Substitution yields

$$\frac{\partial(\tilde{\rho}\overline{u_i u_j})}{\partial x_j} = \frac{\partial\tilde{\rho}(\overline{u_i u_j} + \tau_{ij})}{\partial x_j} = \frac{\partial(\tilde{\rho}\overline{u_i u_j})}{\partial x_j} + \frac{\partial(\tilde{\rho}\tau_{ij})}{\partial x_j}$$

Non-dimensionalizing yields

$$\begin{aligned} \frac{\partial(\tilde{\rho}\overline{u_i u_j})}{\partial x_j} + \frac{\partial(\tilde{\rho}\tau_{ij})}{\partial x_j} &= \frac{\partial(\tilde{\rho}^* \rho_o \overline{u_i^*} U \overline{u_j^*} U)}{\partial x_j^* \ell} + \frac{\partial(\tilde{\rho}^* \rho_o \tau_{ij}^* U^2)}{\partial x_j^* \ell} \\ &= \boxed{\frac{\rho_o U^2}{\ell} \left[\frac{\partial(\tilde{\rho}\overline{u_i u_j})}{\partial x_j} + \frac{\partial(\tilde{\rho}\tau_{ij})}{\partial x_j} \right]} \end{aligned}$$

where we have dropped the * notation for convenience.



- Term 3

$$\frac{\widetilde{\partial p}}{\partial x_i} = \frac{\partial \tilde{p}}{\partial x_i}$$

Non-dimensionalizing yields

$$\frac{\partial \tilde{p}}{\partial x_i} = \frac{\partial \tilde{p}^* \rho_o U^2}{\partial x_i^* \ell} = \boxed{\frac{\rho_o U^2}{\ell} \frac{\partial \tilde{p}}{\partial x_i}}$$

where we have dropped the * notation for convenience.



- Term 4

$$\frac{\partial}{\partial x_j} \left[2\mu S_{ij} - \frac{2}{3}\mu\delta_{ij} \frac{\partial u_k}{\partial x_k} \right]$$

First note that μ is not constant, but rather a function of temperature. So, $\mu = \mu(T)$ and $\bar{\mu} = \mu(\bar{T})$. If we define

$$\sigma_{ij} = 2\mu \left(S_{ij} - \frac{1}{3}\delta_{ij} \frac{\partial u_k}{\partial x_k} \right),$$

then we can rewrite Term 4 as

$$\frac{\partial \sigma_{ij}}{\partial x_j}$$



- Term 4

$$\frac{\partial \widetilde{\sigma}_{ij}}{\partial x_j} = \frac{\partial \widetilde{\sigma}_{ij}}{\partial x_j} = \frac{\partial}{\partial x_j} \left[2\mu \left(S_{ij} - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right) \right]$$

Thus, $\widetilde{\sigma}_{ij}$ cannot be directly expressed in terms of the basic filtered variables

We decompose $\widetilde{\sigma}_{ij}$ into a smooth flow contribution and a subfilter contribution.



Favre-filtered conservation of momentum

- Term 4

$$\text{smooth} \Rightarrow \overline{\sigma_{ij}} = 2\bar{\mu} \left(\bar{S}_{ij} - \frac{1}{3}\delta_{ij} \frac{\partial \bar{u}_k}{\partial x_k} \right)$$

$$\text{subgrid} \Rightarrow \widetilde{\sigma}_{ij} - \overline{\sigma}_{ij}$$

Thus,

$$\frac{\partial \widetilde{\sigma}_{ij}}{\partial x_j} = \frac{\partial \overline{\sigma}_{ij}}{\partial x_j} + \frac{\partial (\widetilde{\sigma}_{ij} - \overline{\sigma}_{ij})}{\partial x_j}$$

Let's non-dimensionalize

$$\frac{\partial \sigma_{ij}}{\partial x_j} = \frac{\partial}{\partial x_j} \left[2\mu \left(S_{ij} - \frac{1}{3}\delta_{ij} \frac{\partial u_k}{\partial x_k} \right) \right]$$

and apply to all of the terms in the above expression.



Favre-filtered conservation of momentum

- Term 4

Recall that $\text{Re} = U\ell/\nu = U\ell\rho_o/\mu_o \Rightarrow \mu_o = U\ell\rho_o/\text{Re}$

$$\mu = \mu^* \mu_o = \frac{\mu^* U \ell \rho_o}{\text{Re}}$$

and

$$S_{ij} = \frac{1}{2} \left(\frac{\partial u_i^* U}{\partial x_j^* \ell} + \frac{\partial u_j^* U}{\partial x_i^* \ell} \right) = \frac{U}{\ell} \frac{1}{2} \left(\frac{\partial u_i^*}{\partial x_j^*} + \frac{\partial u_j^*}{\partial x_i^*} \right) = \frac{U}{\ell} S_{ij}^*$$

and

$$\frac{\partial u_k}{\partial x_k} = \frac{\partial u_k^* U}{\partial x_k^* \ell} = \frac{U}{\ell} \frac{\partial u_k^*}{\partial x_k^*}$$



Favre-filtered conservation of momentum

- Term 4

Putting them altogether yields

$$\begin{aligned}\frac{\partial \sigma_{ij}}{\partial x_j} &= \frac{1}{\ell} \frac{\partial}{\partial x_j^*} \left[2 \frac{\mu^* U \ell \rho_o}{\text{Re}} \left(\frac{U}{\ell} \left\{ S_{ij}^* - \frac{1}{3} \delta_{ij} \frac{\partial u_k^*}{\partial x_k^*} \right\} \right) \right] \\ &= \frac{\rho_o U^2}{\ell} \frac{\partial}{\partial x_j^*} \left[\frac{2\mu^*}{\text{Re}} \left(S_{ij}^* - \frac{1}{3} \delta_{ij} \frac{\partial u_k^*}{\partial x_k^*} \right) \right] \\ &= \frac{\rho_o U^2}{\ell} \frac{\partial \sigma_{ij}^*}{\partial x_j^*}\end{aligned}$$

Thus,

$$\boxed{\frac{\partial \widetilde{\sigma}_{ij}}{\partial x_j} = \frac{\rho_o U^2}{\ell} \frac{\partial \overline{\sigma}_{ij}}{\partial x_j} + \frac{\rho_o U^2}{\ell} \frac{\partial (\widetilde{\sigma}_{ij} - \overline{\sigma}_{ij})}{\partial x_j}}$$

where we have dropped the * notation for convenience.



Favre-filtered conservation of momentum

- Finally, we combine Terms 1-4 and group SFS terms

$$\begin{aligned} & \frac{\rho_o U^2}{\ell} \frac{\partial(\tilde{\rho} \overline{u_i})}{\partial t} + \frac{\rho_o U^2}{\ell} \frac{\partial(\tilde{\rho} \overline{u_i} \overline{u_j})}{\partial x_j} + \frac{\rho_o U^2}{\ell} \frac{\partial \tilde{p}}{\partial x_i} - \frac{\rho_o U^2}{\ell} \frac{\partial \overline{\sigma_{ij}}}{\partial x_j} \\ & = - \frac{\rho_o U^2}{\ell} \frac{\partial(\tilde{\rho} \tau_{ij})}{\partial x_j} + \frac{\rho_o U^2}{\ell} \frac{\partial(\tilde{\sigma}_{ij} - \overline{\sigma_{ij}})}{\partial x_j} \end{aligned}$$

Cancelling $\rho_o U^2 / \ell$ yields the dimensionless Favre-filtered conservation of momentum equation

$$\boxed{\frac{\partial(\tilde{\rho} \overline{u_i})}{\partial t} + \frac{\partial(\tilde{\rho} \overline{u_i} \overline{u_j})}{\partial x_j} + \frac{\partial \tilde{p}}{\partial x_i} - \frac{\partial \overline{\sigma_{ij}}}{\partial x_j} = - \frac{\partial(\tilde{\rho} \tau_{ij})}{\partial x_j} + \frac{\partial(\tilde{\sigma}_{ij} - \overline{\sigma_{ij}})}{\partial x_j}}$$



Favre-filtered conservation of momentum

$$\frac{\partial(\tilde{\rho}\overline{u_i})}{\partial t} + \frac{\partial(\tilde{\rho}\overline{u_i u_j})}{\partial x_j} + \frac{\partial\tilde{p}}{\partial x_i} - \frac{\partial\overline{\sigma_{ij}}}{\partial x_j} = -\frac{\partial(\tilde{\rho}\tau_{ij})}{\partial x_j} + \frac{\partial(\tilde{\sigma}_{ij} - \overline{\sigma_{ij}})}{\partial x_j}$$

The terms comprising the SFS viscous term on the RHS are:

- “smooth” viscous stress tensor

$$\overline{\sigma_{ij}} = \frac{2}{\text{Re}} \bar{\mu} \left(\bar{S}_{ij} - \frac{1}{3} \delta_{ij} \frac{\partial \overline{u_k}}{\partial x_k} \right)$$

- non-linear viscous stress tensor

$$\tilde{\sigma}_{ij} = \frac{2}{\text{Re}} \mu \left(S_{ij} - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right)$$



Favre-filtered kinetic energy equation

- The full kinetic energy equation is written as

$$\frac{\partial e}{\partial t} + \frac{\partial}{\partial x_j} [(e + p)u_j] - \frac{\partial(u_i \sigma_{ij})}{\partial x_j} + \frac{\partial q_j}{\partial x_j} = 0$$

- e is the total energy density

$$e = \frac{p}{\gamma - 1} + \frac{1}{2} \rho u_i u_i \quad \text{where} \quad \gamma = \frac{c_p}{c_v} \approx 1.4 \text{ for air}$$

- σ_{ij} is the viscous stress tensor

$$\frac{2\mu}{\text{Re}} \left(S_{ij} - \frac{1}{3} \delta_{ij} \frac{\partial u_k}{\partial x_k} \right)$$



Favre-filtered kinetic energy equation

- The full kinetic energy equation is written as

$$\frac{\partial e}{\partial t} + \frac{\partial([e + p)u_j]}{\partial x_j} - \frac{\partial(u_i \sigma_{ij})}{\partial x_j} + \frac{\partial q_j}{\partial x_j} = 0$$

- q_j is the heat flux

$$q_j = -\frac{\mu}{(\gamma - 1)\text{RePr}M^2} \frac{\partial T}{\partial x_j}$$

where Pr is the Prandtl number (≈ 0.72 for air) and M is the reference Mach number:

$$M = \frac{U}{c} \quad \text{where} \quad c = \sqrt{\gamma RT}$$

and R is the ideal gas law constant.



Favre-filtered kinetic energy equation

- Applying the Favre filter to this equation is left as an exercise for you.
- The resulting Favre-filtered kinetic energy equation is given by

$$\frac{\partial \bar{e}}{\partial t} + \frac{\partial [(\bar{e} + \tilde{p})\bar{u}_j]}{\partial x_j} - \frac{(\bar{u}_i \bar{\sigma}_{ij})}{\partial x_j} + \frac{\partial \bar{q}_j}{\partial x_j} = -a_1 - a_2 - a_3 + a_4 + a_5 - a_6$$



Favre-filtered kinetic energy equation

$$\frac{\partial \bar{e}}{\partial t} + \frac{\partial [(\bar{e} + \tilde{p})\bar{u}_j]}{\partial x_j} - \frac{(\bar{u}_i \bar{\sigma}_{ij})}{\partial x_j} + \frac{\partial \bar{q}_j}{\partial x_j} = -a_1 - a_2 - a_3 + a_4 + a_5 - a_6$$

$$a_1 = \bar{u}_i \frac{\partial (\tilde{p}\tau_{ij})}{\partial x_j} \Rightarrow \text{kinetic energy transferred from resolved to SFSs}$$

$$a_2 = \frac{1}{\gamma - 1} \frac{\widetilde{p\bar{u}_j} - \tilde{p}\bar{u}_j}{\partial x_j} \Rightarrow \text{pressure velocity SFS term (effect of SFS turbulence on the conduction of heat at resolved scales)}$$

$$a_3 = p \frac{\widetilde{\partial u_j}}{\partial x_j} - \tilde{p} \frac{\partial \bar{u}_j}{\partial x_j} \Rightarrow \text{compressibility effects (vanishes for incompressible)}$$



Favre-filtered kinetic energy equation

$$\frac{\partial \bar{e}}{\partial t} + \frac{\partial [(\bar{e} + \tilde{p})\bar{u}_j]}{\partial x_j} - \frac{(\bar{u}_i \bar{\sigma}_{ij})}{\partial x_j} + \frac{\partial \bar{q}_j}{\partial x_j} = -a_1 - a_2 - a_3 + a_4 + a_5 - a_6$$

$$a_4 = \overbrace{\sigma_{ij} \frac{\partial u_i}{\partial x_j}} - \tilde{\sigma}_{ij} \frac{\partial \bar{u}_i}{\partial x_j} \Rightarrow \text{conversion of SFS kinetic energy to internal energy by viscous dissipation}$$

$$a_5 = \frac{\partial (\tilde{\sigma}_{ij} \bar{u}_i - \bar{\sigma}_{ij} \bar{u}_i)}{\partial x_j} \Rightarrow \text{SFS viscous stress term}$$

$$a_6 = \frac{\partial (\tilde{q}_j - \bar{q}_j)}{\partial x_j} \Rightarrow \text{SFS heat flux term}$$

It is typically assumed that $\tilde{\sigma}_{ij} - \bar{\sigma}_{ij} \approx 0$ and $\tilde{q}_j - \bar{q}_j \approx 0$. This eliminates terms a_5 and a_6 .

