Environmental Fluid Dynamics: Lecture 11

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Overview

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Scale Analysis

Conservation of Momentum:

Conservation of Momentum: Scale Analysis

 We showed that the vector equation of motion in a non-inertial (rotating) reference frame is

$$\underbrace{\frac{D\vec{U}}{Dt}}_{1} = \underbrace{-\frac{1}{\rho}\vec{\nabla}p}_{2} \underbrace{-2\vec{\Omega}\times\vec{U}}_{3} + \underbrace{\vec{g}}_{4} + \underbrace{\nu\vec{\nabla}^{2}\vec{U}}_{5}$$

where

- 1 acceleration in rotating coordinate system
- pressure gradient force
- Coriolis
- 4 effective gravity
- fric tion



Conservation of Momentum: Scale Analysis

- It is useful to understand the momentum balance equation at various dominant scales in the atmosphere.
- Scale analysis is a very useful method for establishing the importance of various processes in the atmosphere and terms in the governing equations.
- Based on the relative importance of these processes/terms, we can deduce the behavior of motion at such scales.

Conservation of Momentum: Scale Analysis

- Scale analysis makes use of order-of-magnitude reasoning.
- First, we assign a characteristic value for each of the governing variables.
- Next, we use these characteristic values to estimate the magnitude of each term.
- We then compare terms to determine their relative importance.
- Based on which terms are most important, we can describe the approximate flow behavior at a particular scale.



- To simplify things, let's assume mid-latitude ($\phi=45^\circ$)
- We can then define the Coriolis parameter as $f = 2\Omega \sin \phi = 2\Omega \cos \phi$
- We will also make use of the f-plane assumption (f=const).
- Frictional effects are ignored (check for yourself the viscous term is many orders of magnitude smaller than the dominant terms in each equation).
- Just to emphasize: the typical magnitude of change defines the scale, which is not always the same as the magnitude of the quantity itself.



The typical scales in the horizontal momentum equation for the *synoptic scale* are:

- $V \sim 10 \text{ ms}^{-1}$
- $W \sim 0.1 \; {\rm ms}^{-1}$
- $L \sim 1000 \text{ km} = 10^6 \text{ m}$
- $H \sim 10 \text{ km} = 10^4 \text{ m}$
- $T \sim L/V \sim 10^5 \text{ s}$
- $f \sim 10^{-4} \text{ s}^{-1}$
- $\rho \sim 1 \text{ kg m}^{-3}$
- Δp in horizontal $\sim 10 \text{ mb} = 1000 \text{ Pa}$
- Δp over vertical length scale $H \sim 1000~\mathrm{mb} = 10^5~\mathrm{Pa}$



Apply the typical scales to the u-component of velocity:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + fv$$

$$\frac{V}{T}$$
 $\frac{VV}{L}$ $\frac{VV}{L}$ $\frac{WV}{H}$ $\frac{\Delta p}{\rho L}$ fV

$$\frac{10}{10^5} \qquad \frac{10 \times 10}{10^6} \qquad \frac{10 \times 10}{10^6} \qquad \frac{0.1 \times 10}{10^4} \qquad \frac{10^3}{1 \times 10^6} \qquad 10^{-4} \times 10$$

$$10^{-4} 10^{-4} 10^{-4} 10^{-4} 10^{-3} 10^{-3}$$

Apply the typical scales to the w-component of velocity:

$$\frac{\partial w}{\partial t} - + u \frac{\partial w}{\partial x} - v \frac{\partial w}{\partial y} - w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g$$

$$\frac{W}{T}$$
 $\frac{VW}{L}$ $\frac{VW}{L}$ $\frac{WW}{H}$ $\frac{\Delta p}{\rho H}$ g

$$\frac{0.1}{10^5} \qquad \frac{10 \times 0.1}{10^6} \qquad \frac{10 \times 0.1}{10^6} \qquad \frac{0.1 \times 0.1}{10^4} \qquad \frac{10^5}{1 \times 10^4} \qquad 10$$

$$10^{-6} 10^{-6} 10^{-6} 10^{-6} 10$$



- For horizontal motions, the pressure gradient force and Coriolis are the two dominant scales.
- For vertical motions, the pressure gradient force and gravity are the two dominant scales.
- The flow is quasi-two-dimensional (because w << u)
- The flow is roughly hydrostatic
- The flow is quasi-geostrophic

The typical scales in the horizontal momentum equation for the *mesoscale* are:

- $V \sim 10 \text{ ms}^{-1}$
- $W \sim 1 \text{ ms}^{-1} (\uparrow)$
- $L \sim 100 \text{ km} = 10^5 \text{ m} (\downarrow)$
- $H \sim 10 \text{ km} = 10^4 \text{ m}$
- $T \sim L/V = 10^4 \text{ s } (\downarrow)$
- $f \sim 10^{-4} \text{ s}^{-1}$
- $\rho \sim 1 \text{ kg m}^{-3}$
- Δp in horizontal $\sim 1~\mathrm{mb} = 100~\mathrm{Pa}~(\downarrow)$
- Δp over vertical length scale $H \sim 1000~\mathrm{mb} = 10^5~\mathrm{Pa}$



Apply the typical scales to the u-component of velocity:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + fv$$

$$\frac{V}{T} \frac{VV}{L} \frac{VV}{L} \frac{WV}{L} \frac{\Delta p}{H} \frac{fV}{\rho L}$$

$$\frac{10}{10^4} \qquad \frac{10 \times 10}{10^5} \qquad \frac{10 \times 10}{10^5} \qquad \frac{1 \times 10}{10^4} \qquad \frac{10^2}{1 \times 10^5} \qquad 10^{-4} \times 10$$

$$10^{-3} 10^{-3} 10^{-3} 10^{-3} 10^{-3} 10^{-3}$$

Apply the typical scales to the w-component of velocity:

$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial z} - g$$

$$\frac{W}{T} \frac{VW}{L} \frac{VW}{L} \frac{WW}{L} \frac{WW}{H} \frac{\Delta p}{\rho H} g$$

$$\frac{1}{10^4} \frac{10 \times 1}{10^5} \frac{10 \times 1}{10^5} \frac{1 \times 1}{10^4} \frac{10^5}{1 \times 10^4} 10$$

$$10^{-4} 10^{-4} 10^{-4} 10^{-4} 10$$



- For horizontal motions, all terms in the equation are of the same magnitude (none of them can be neglected) and We no longer have geostrophy!
- For vertical motions, the pressure gradient force and gravity are the two dominant scales.
- ullet The flow is quasi-two-dimensional (because w << u)
- The flow is roughly hydrostatic
- The flow is non-geostrophic

The typical scales in the horizontal momentum equation for the *mesoscale* are:

- $V \sim 10 \text{ ms}^{-1}$
- $W \sim 10 \text{ ms}^{-1} (\uparrow)$
- $L \sim 10 \text{ km} = 10^4 \text{ m} (\downarrow)$
- $H \sim 10 \text{ km} = 10^4 \text{ m}$
- $T \sim L/V = 10^3 \text{ s } (\downarrow)$
- $f \sim 10^{-4} \text{ s}^{-1}$
- $\rho \sim 1 \text{ kg m}^{-3}$
- Δp in horizontal $\sim 1~\mathrm{mb} = 100~\mathrm{Pa}$
- Δp over vertical length scale $H \sim 1000~\mathrm{mb} = 10^5~\mathrm{Pa}$



Apply the typical scales to the u-component of velocity:

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial x} + v \frac{\partial u}{\partial y} + w \frac{\partial u}{\partial z} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + fv$$

$$rac{V}{V}$$
 $rac{VV}{V}$ $rac{VV}{V}$ $rac{WV}{V}$ $rac{\Delta p}{fV}$

$$\frac{V}{T}$$
 $\frac{VV}{L}$ $\frac{VV}{L}$ $\frac{WV}{H}$ $\frac{\Delta p}{\rho L}$ fV

$$\frac{10}{10^3} \qquad \frac{10 \times 10}{10^4} \qquad \frac{10 \times 10}{10^4} \qquad \frac{10 \times 10}{10^4} \qquad \frac{10^2}{1 \times 10^4} \qquad 10^{-4} \times 10$$

$$10^{-2} 10^{-2} 10^{-2} 10^{-2} 10^{-2} 10^{-3}$$

Apply the typical scales to the w-component of velocity - which are now based on the Bousinessq equations of motion.

- $\nabla \cdot \vec{u} \approx 0$
- ullet ho= constant everywhere, except when paired with gravity
- viscosity, thermal diffusivity, and specific heat are assumed constant

The Boussinesq approximation is used because it is the residual between the PGF and buoyancy force terms. Therefore we want to estimate the terms in terms of the deviations/perturbations from the hydrostatically balanced base state.

Apply the typical scales to the w-component of velocity:

$$\frac{\partial w}{\partial t} + u \frac{\partial w}{\partial x} + v \frac{\partial w}{\partial y} + w \frac{\partial w}{\partial z} = -\frac{1}{\overline{\rho}} \frac{\partial p'}{\partial z} + \frac{\theta'}{\overline{\theta}} g$$

$$\partial t$$
 ∂x ∂y ∂z $\overline{\rho} \partial z$ $\overline{\theta}$ $\partial \theta$ $\partial \theta$

$$\frac{W}{T}$$
 $\frac{VW}{L}$ $\frac{VW}{L}$ $\frac{WW}{H}$ $\frac{\Delta p}{\overline{\rho}H}$ $\frac{\Delta \theta}{\theta_0}g$

$$\frac{10}{10^3} \qquad \frac{10 \times 10}{10^4} \qquad \frac{10 \times 10}{10^4} \qquad \frac{10 \times 10}{10^4} \qquad \frac{10^2}{0.5 \times 10^4} \qquad \frac{1 \times 10}{300}$$

$$10^{-2}$$
 10^{-2} 10^{-2} 10^{-2} 2×10^{-2} 3×10^{-2}



- For horizontal motions, all terms in the equation are of the same magnitude except Coriolis, which can be neglected.
- For vertical motions, all terms in the equation are of the same magnitude (none of them can be neglected)!
- The flow is three-dimensional $(u \sim w)$
- The flow is nonhydrostatic
- The flow is ageostrophic

Conservation of Momentum:

Approximations and Simplifications

 We first examined large (synoptic) scales, focusing on the horizontal components

$$\frac{Du}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial x} + 2\Omega v \sin \phi - 2\Omega w \cos \phi + \nu \vec{\nabla}^2 u + g_x$$

$$\frac{Dv}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial y} - 2\Omega u \sin \phi + \nu \vec{\nabla}^2 v + g_y$$

- We defined the Coriolis parameter ($f=2\Omega\sin\phi$) and assumed mid-latitude ($\phi=45^\circ$; a.k.a. the f-plane assumption since f is constant)
- Assumed steady-state $(\partial u/\partial t = 0)$ and neglected non-linear terms $(u \ \partial u/\partial x + ... = 0)$
- ullet Assumed $U\gg W$ and aligned gravity with $\hat{m k}$
- Neglected frictional effects



- The resulting expression is a balance between Coriolis and the pressure gradient force in the horizontal direction
- This balance is called the geostrophic approximation

$$-fv = -\frac{1}{\rho} \frac{\partial p}{\partial x}$$
$$fu = -\frac{1}{\rho} \frac{\partial p}{\partial y}$$

 The geostrophic balance is a diagnostic expression (no time derivatives) that gives the relationship between the pressure field and horizontal wind in large-scale systems



 We can now define a horizontal wind that satisfies the geostrophic approximation - called the geostrophic wind

$$-fv = -\frac{1}{\rho} \frac{\partial p}{\partial x} \Rightarrow v_g = \frac{1}{f\rho} \frac{\partial p}{\partial x}$$
$$fu = -\frac{1}{\rho} \frac{\partial p}{\partial y} \Rightarrow u_g = -\frac{1}{f\rho} \frac{\partial p}{\partial y}$$

Combining yields

$$ec{V}_g \equiv u_g \hat{\pmb{\imath}} + v_g \hat{\pmb{\jmath}}$$
 $ec{V}_g \equiv \hat{\pmb{k}} imes rac{1}{f
ho} \vec{\nabla} p$



$$ec{V}_g \equiv \hat{m{k}} imes rac{1}{f
ho} ec{
abla} p$$

- Thus, if we know the distribution of the pressure field then we know the geostrophic wind
- Remember, this is only valid for quasi-steady, large-scale motions away from the equator (at equator, $\phi=0 \to \sin\phi=0 \to f=0) \text{ and above the PBL (w/in PBL, friction and vertical momentum exchange are important)}$
- \bullet For synoptic scales, the geostrophic wind is within 10-15% of the actual horizontal wind



$$-fv = -\frac{1}{\rho}\frac{\partial p}{\partial x}$$
 $fu = -\frac{1}{\rho}\frac{\partial p}{\partial y}$

• These expressions imply that $\vec{V}_g \cdot \vec{\nabla} p = 0$ (i.e., $\vec{V}_g \perp \vec{\nabla} p$)

$$(u_g \hat{\imath} + v_g \hat{\jmath}) \cdot (\frac{\partial p}{\partial x} \hat{\imath} + \frac{\partial p}{\partial y} \hat{\jmath}) = u_g \frac{\partial p}{\partial x} + v_g \frac{\partial p}{\partial y}$$

Recall that

$$u_g = -\frac{1}{f\rho} \frac{\partial p}{\partial y}$$
 $v_g = \frac{1}{f\rho} \frac{\partial p}{\partial x}$

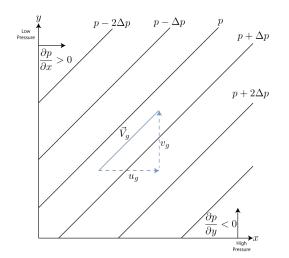
Substitution yields

$$-\frac{1}{f\rho}\frac{\partial p}{\partial y}\frac{\partial p}{\partial x} + \frac{1}{f\rho}\frac{\partial p}{\partial x}\frac{\partial p}{\partial y} = 0$$

Thus, $ec{V}_g \parallel$ to lines of constant pressure



 \bullet Since, $\vec{V}_g \parallel$ to lines of constant pressure, that means isobars on a weather map are nearly streamlines





 If we want to develop a prognostic equation using the geostrophic approximation, we must retain the acceleration term

$$\frac{Du}{Dt} = fv - \frac{1}{\rho} \frac{\partial p}{\partial x}$$
$$\frac{Dv}{Dt} = -fu - \frac{1}{\rho} \frac{\partial p}{\partial y}$$

Recall that

$$u_g = -\frac{1}{f\rho} \frac{\partial p}{\partial y}$$
 $v_g = \frac{1}{f\rho} \frac{\partial p}{\partial x}$

Substitution yields

$$\frac{Du}{Dt} = f(v - v_g)$$

$$\frac{Dv}{Dt} = -f(u - u_g)$$

• In other words, accelerations are proportional to the departure of the wind from the geostrophic wind



$$\frac{Du}{Dt} = f(v - v_g)$$
 $\frac{Dv}{Dt} = -f(u - u_g)$

- If you recall from scale analysis, the acceleration terms are an order of magnitude smaller than the Coriolis and pressure terms
- While geostrophic balance is a useful diagnosis tool, its application to weather forecasting is fraught with difficulty
- Why? The acceleration (very important to get right) is equal to the small difference between two large terms - which means it is susceptible to measurement errors in velocity or pressure gradient



 A useful comparison of the magnitude of the acceleration with the Coriolis force is through the ratio of their respective characteristic scales

$$\frac{U^2/L}{f_o L}$$

This non-dimensional number is called the Rossby NUmber

$$Ro \equiv \frac{U}{f_o L}$$

- Named after Swedish meteorologist Carl-Gustav Rossby
- As Ro becomes smaller, rotational effects are more important and the geostrophic approximation is more valid
- ullet Ro breaks down near the equator, where f
 ightarrow 0



Hydrostatic Approximation

 Next, we examined large (synoptic) scales and applied scale analysis to the vertical component

$$\frac{Dw}{Dt} = -\frac{1}{\rho} \frac{\partial p}{\partial z} + 2\Omega u \cos \phi + \nu \vec{\nabla}^2 w + g_z$$

- We assumed mid-latitude, steady-state, and neglected non-linear terms and frictional effects
- Assumed $U\gg W$ and aligned gravity with $\hat{m k}$



Hydrostatic Approximation

- The resulting expression is a balance between the vertical pressure gradient and gravity
- This balance is called the hydrostatic approximation

$$\frac{\partial p}{\partial z} = -\rho g$$

- This expression can be related to the hypsometric equation (see Lecture 5)
- In other words, vertical accelerations are small compared to gravity at large scales and so the pressure at any point is equal to the weight of the overlying air



- This is really 3 assumptions motivated byt he fact that compressibility effects are often small for atmospheric flows
 - **1** Assume flow is incompressible: $\vec{\nabla} \cdot \vec{U} = 0$
 - Material properties (viscosity, thermal diffusivity, and specific heat) are assumed constant
 - Oensity is allowed to vary in gravity term but not in inertia term
- Let's look at assumption 3



- In reality, ρ may vary in (x, y, z, t)
- We want to approximate it based on the smallness of its deviation from the mean
- Define a base-state pressure based on constant density ρ_0 (i.e., reference atmosphere has constant density)

$$\rho = \rho_0 + \rho'$$

Then

$$p = \bar{p} + p'$$

where \bar{p} is the solutions of $\partial \bar{p}/\partial z = -\rho_0 g$



The equations of motion become

$$(\rho_0 + \rho') \frac{D\vec{U}}{Dt} = -\vec{\nabla}p' \underbrace{-\vec{\nabla}\bar{p} - \rho_0 g\hat{k}}_{\text{These cancel}} - \rho'g\hat{k} + \mu\vec{\nabla}^2\vec{U}$$

divide by ρ_0

$$\left(1 + \frac{\rho'}{\rho_0}\right) \frac{D\vec{U}}{Dt} = -\frac{1}{\rho_0} \vec{\nabla} p' - \frac{\rho'}{\rho_0} g \hat{k} + \nu \vec{\nabla} \vec{U}$$

Assume $\rho'/\rho_0 \ll 1$, so finally

$$\frac{D\vec{U}}{Dt} = -\frac{1}{\rho_0}\vec{\nabla}p' - \frac{\rho'}{\rho_0}g\hat{k} + \nu\vec{\nabla}\vec{U}$$



• Now let's consider the term $\rho^{'}/\rho$. The equation of state is given by $p=\rho RT$, which is decomposed as

$$\frac{\overline{p}}{R} + \frac{p'}{R} = \overline{\rho} \ \overline{T} + \overline{\rho} T' + \rho' \overline{T} + \rho' T'$$

Next, we apply Reynolds averaging

$$\frac{\overline{\overline{p}}}{R} + \frac{\overline{p'}}{R} = \overline{\overline{\rho}} \, \overline{\overline{T}} + \overline{\overline{\rho}} \overline{T'} + \overline{\overline{\rho'}} \overline{\overline{T}} + \overline{\overline{\rho'}} \overline{T'} \longrightarrow \frac{\overline{\overline{p}}}{R} = \overline{\overline{\rho}} \, \overline{T} + \overline{\overline{\rho'}} \overline{T'} \longrightarrow \frac{\overline{\overline{p}}}{R} = \overline{\overline{\rho}} \, \overline{T}$$

 Thus, the equation of state holds in the mean. This is reasonable because the equation of state was originally formulated from measurements made with crude, slow-response sensors. These sensors were essentially measuring mean quantities.



 Now let's subtract the mean equation of state from the full linearized form

$$\frac{\overline{p}}{R} + \frac{p'}{R} - \frac{\overline{p}}{R} = \overline{\rho} \, \overline{T} + \overline{\rho} T' + \rho' \overline{T} + \rho' T' - \overline{\rho} \, \overline{T} \longrightarrow \frac{p'}{R} = \overline{\rho} T' + \rho' \overline{T} + \rho' T'.$$

Finally divide by the mean equation of state

$$\frac{p^{'}R}{R\overline{p}} = \frac{\overline{\rho}}{\overline{\rho}}\frac{T^{'}}{\overline{T}} + \frac{\rho^{'}\overline{T}}{\overline{\rho}}\frac{\overline{T}}{\overline{T}} + \frac{\rho^{'}T^{'}}{\overline{\rho}}\frac{T^{'}}{\overline{T}} \longrightarrow \frac{p^{'}}{\overline{p}} = \frac{\rho^{'}}{\overline{\rho}} + \frac{T^{'}}{\overline{T}} + \frac{\rho^{'}T^{'}}{\overline{\rho}}\frac{T^{'}}{\overline{T}}.$$

 The last term is much smaller than the others is safely neglected, which leads to

$$\frac{p^{'}}{\overline{p}} = \frac{\rho^{'}}{\overline{\rho}} + \frac{T^{'}}{\overline{T}} \; .$$



$$\frac{p'}{\overline{p}} = \frac{\rho'}{\overline{\rho}} + \frac{T'}{\overline{T}} .$$

• This is the linearized perturbation ideal gas law. Scale analysis shows that $p'/\overline{p} \to 0.1~\mathrm{hPa}/1000~\mathrm{hPa} = 10^{-4}$, while $T'/\overline{T} \to 1~\mathrm{K}/300~\mathrm{K} = 3.33^{-3}$. Thus, we can neglect the pressure term, yielding

$$\frac{\rho^{'}}{\overline{\rho}}\approx -\frac{T^{'}}{\overline{T}}$$



 Recalling that $T^{'}=T-\overline{T}$ and making use of the Poisson equation, one can write

$$\frac{T^{'}}{\overline{T}} = \frac{\theta \left(\frac{p}{p_{0}}\right)^{\frac{R}{c_{p}}} - \overline{\theta} \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}}}{\overline{\theta} \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}}} = \frac{\theta \left(\frac{\overline{p} + p^{'}}{p_{0}}\right)^{\frac{R}{c_{p}}} - \overline{\theta} \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}}}{\overline{\theta} \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}}} \approx \frac{\theta \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}} - \overline{\theta} \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}}}{\overline{\theta} \left(\frac{\overline{p}}{p_{0}}\right)^{\frac{R}{c_{p}}}} \approx \frac{\theta - \overline{\theta}}{\overline{\theta}}.$$



Thus, one can use the approximation that

$$\boxed{\frac{\rho^{'}}{\overline{\rho}} \approx -\frac{T^{'}}{\overline{T}} \approx -\frac{\theta^{'}}{\overline{\theta}}}$$

 We can use this approximation, we can write the equations of motion in terms of buoyancy

$$\frac{D\vec{U}}{Dt} = -\frac{1}{\rho_0} \vec{\nabla} p' + \beta \theta' + \nu \vec{\nabla} \vec{U}$$

where $\beta=g\hat{m k}/\overline{ heta}$ is the buoyancy parameter



We can rewrite this expression by noting that

$$\frac{1}{\rho_0}\vec{\nabla}p' = \frac{1}{\rho_0}\vec{\nabla}p - \frac{1}{\rho_0}\vec{\nabla}\bar{p}$$

where

$$\frac{1}{\rho_0}\vec{\nabla}\bar{p} = -g\hat{k}$$

Combined, we can write the equations of motion as

$$\frac{D\vec{U}}{Dt} = \frac{1}{\rho_0} \vec{\nabla} p - g\hat{k} + \beta \theta' + \nu \vec{\nabla} \vec{U}$$



$$\frac{D\vec{U}}{Dt} = \frac{1}{\rho_0} \vec{\nabla} p - g\hat{k} + \beta \theta' + \nu \vec{\nabla} \vec{U}$$

- The Boussinesq approximation essentially describes the residual between the pressure gradient force and the buoyancy force
- This is why we estimate in terms of deviations/perturbation from the hydrostatically-balanced base state